

# *Lightweight, Scalable Manufacturing of Telescope Optics*

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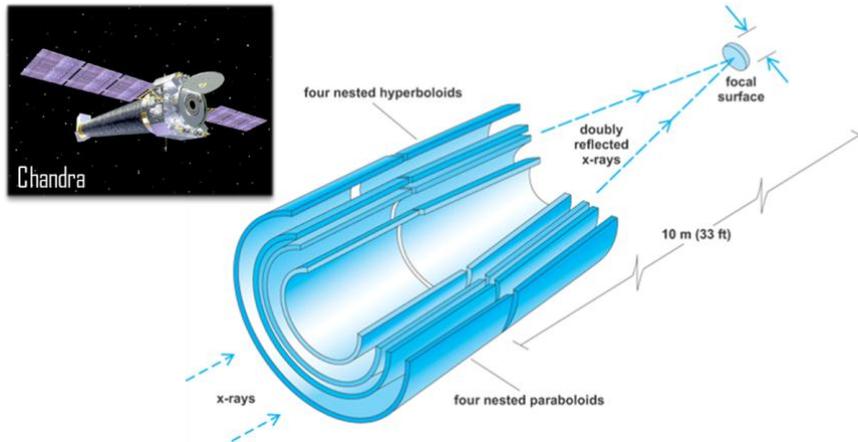
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## Need for Lightweight Telescope Optics

- Decrease the weight of current Wolter Type I optics to allow for greater shell packing and thus increase effective X-ray collection area (i.e. increase the optical surface area per unit mass)
- Reduce the requirements and cost of telescope launch vehicle

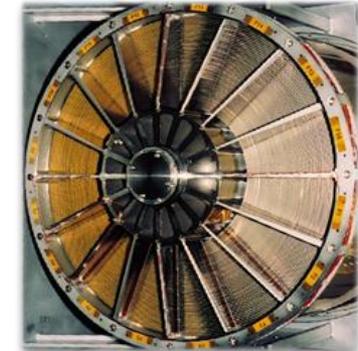


Chandra X-ray observatory utilizing 4 nested zerodur optics with the outer shell measuring 1.2 meters in diameter.

Cross sectional view of Wolter I optic showing grazing angle reflection and nested reflector capability



XMM Newton



Current State of the Art X-ray observatory (XMM Newton) utilizing 58 nested reflector shells; largest reflector 70cm diameter.

Note the increased number of shells compared to that of Chandra resulting in greater optical area and thus greater X-ray collection

## Benefit of Electroformed Optic

- Individual mirror thickness reduced by greater than an order of magnitude (1mm vs. 20mm)
- Reduced mirror thickness allow for a greater number of shells to be nested

## Disadvantage of Electroformed Optic

- Density of Ni compared to zerodur
- Figure accuracy not as good as zerodur

## Electroformed nickel replication (ENR)

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Repeat



### Benefit of the Electroforming Process

- Well suited for precision replication (widely used in optical manufacturing)
- Superpolished mandrel is reuseable, can be “touched up” as necessary

### Disadvantage of Electroformed Optic

- Density of Ni compared to zerodur ( $8.9\text{g/cm}^3$  vs  $2.5\text{g/cm}^3$ )
- Figure accuracy not as good as zerodur

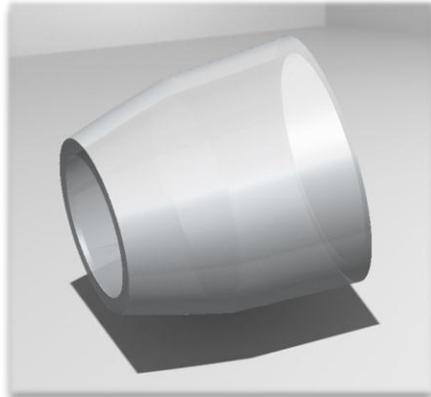
**NiCo alone is too heavy for X-ray telescope missions**

**There exists a need to replace much of the NiCo with a less dense material**



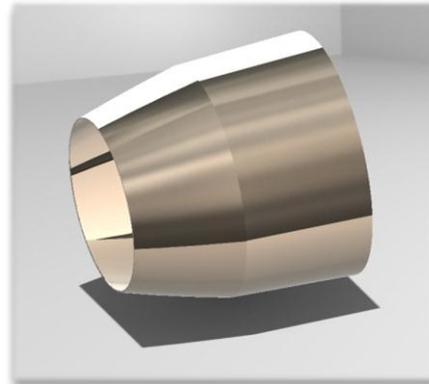
# Telescope Optics: Proposed Innovation

## Current Standard



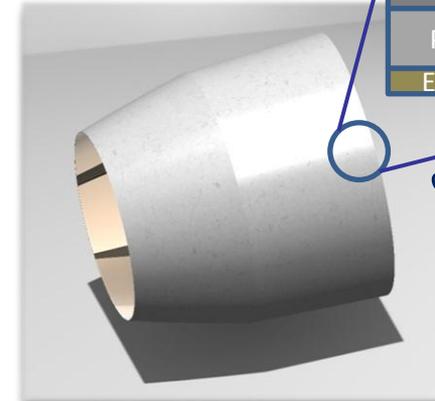
20mm Zerodur

## Current State of the Art



1mm NiCo

## Proposed Innovation



$\leq 100\mu\text{m}$  NiCo  
 $200\mu\text{m}$   $\text{Al}_2\text{O}_3$

Dense  $\text{Al}/\text{Al}_2\text{O}_3$

Porous  $\text{Al}/\text{Al}_2\text{O}_3$

Electroformed Ni

cross section

**Thickness of NiCo remains constant as shell diameter increases**

**Comparison : Mass of Wolter I Optic with a 70cm diameter, 60cm long**

**68.7 kg**

**11.8 kg**

**1.9 kg**

## Proposed Innovation

- Replace zerodur optic with NiCo shell and thermal spray ceramic support structure
- Utilize NiCo electroforming to replicate the surface micro-roughness of the mandrel
- Combine a graded-density lightweight ceramic support coating to hold figure accuracy and supply rigidity for handling



## Thermal Spray Processes

Twin Wire  
Arc

Flame /  
Combustion

Atmospheric  
Plasma Spray

High Velocity  
Oxy Fuel

Cold  
Spray

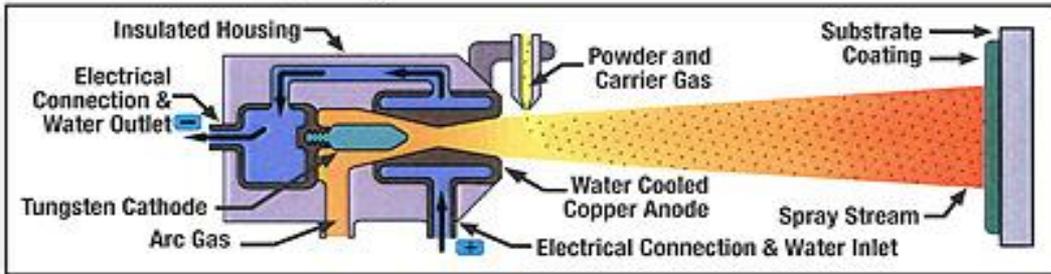
Detonation  
Spray

### Plasma Spray Process

[http://www.thermalspray.org/site\\_plasmaarc.asp](http://www.thermalspray.org/site_plasmaarc.asp)

© 2005 International Thermal Spray Association

Associated with more than 100 variables



Characteristics	
Flame Temperature:	Approximately 12,000 - 20,000°F (6,000 - 11,100°C)
Gases Used:	Ar/H <sub>2</sub> N <sub>2</sub> /H <sub>2</sub>
Particle Speed:	800 - 1,800 ft/s (240-550 m/s)

Photo Courtesy of Westaim Ambeon

- Spray Conditions:**
- Torch Settings
  - Powder
  - Substrate Condition
  - Spray Pattern

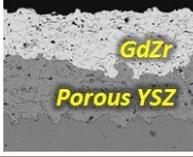
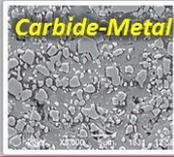
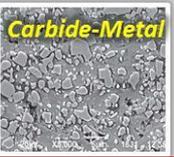
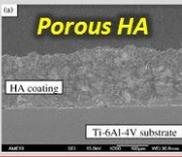
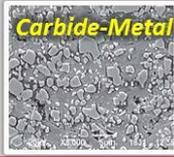
- In Flight Particles:**
- Temperature
  - Velocity
  - Trajectory
- 

- Coating Build-up:**
- Splat Morphology
  - Microstructure
  - Porosity
  - Interlamellar Contact

- Properties:**
- Mechanical
  - Thermal
  - Reliability
- 



## Wide Range of Thermal Spray Coated Components

<p><b>APPLICATIONS</b></p>	<p>Energy - Gas Turbine Engine</p> 	<p>Industrial machinery</p> 	<p>Aviation Engine / Landing Gear</p> 	<p>Bio-implants</p> 	<p>Metal / Paper Manufacturing</p> 	<p>Electronics Manufacturing</p> 
<p><b>Thermal Spray Processes</b></p>	 <p>APS</p>	 <p>HVOF</p>	 <p>HVOF</p>	 <p>APS</p>	 <p>HVOF</p>	 <p>APS</p>
<p><b>COATING MATERIAL &amp; MICROSTRUCTURE</b></p>	 <p>GdZr Porous YSZ</p>	 <p>Carbide-Metal</p>	 <p>Carbide-Metal</p>	 <p>Porous HA HA coating Ti-6Al-4V substrate</p>	 <p>Carbide-Metal</p>	 <p>Dense YSZ</p>
<p><b>PHYSICAL CHARACTERISTICS</b></p>	<p>Thickness Weight Porosity</p>	<p>Thickness Crack Porosity</p>	<p>Thickness Crack Weight</p>	<p>Thickness Defect Density Roughness</p>	<p>Thickness Crack Roughness</p>	<p>Thickness Defect Density</p>
<p><b>PROPERTIES &amp; PERFORMANCES</b></p>	<p>Residual Stress Adhesion Sintering/Aging Conductivity Toughness</p>	<p>Residual Stress Adhesion Strength Toughness Wear</p>	<p>Residual Stress Adhesion Strength Toughness Wear</p>	<p>Residual Stress Adhesion Toughness Phase Stability</p>	<p>Residual Stress Adhesion Strength Toughness Wear</p>	<p>Residual Stress Adhesion Erosion Phase Stability Thermal Expansion</p>



# Why Thermal Spray for this Application?

## Materials Selection

- Wide array of materials to select from
  - Metals, ceramics, polymers, composites
- Ability to tailor the material to not only match the expansion but also provide compliance via defects (thermal cycling compliance)

## Process Parameters

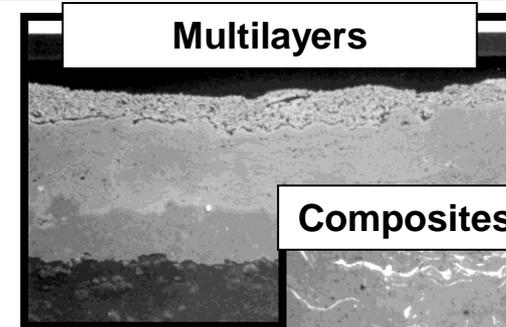
- Ability to tailor the microstructure, density, and interface through use of graded layers
- Ability to control deposition temperature
  - Robot raster speed
  - Secondary cooling



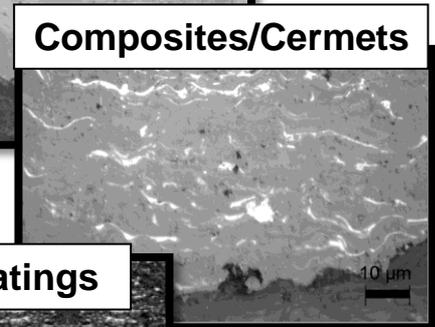
NiAl deposited onto canvas

## Component Manufacturing

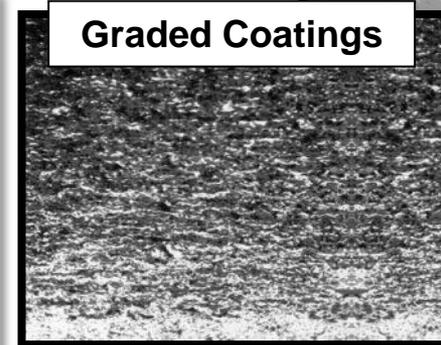
- Ability to deposit onto large cylindrical geometries
  - Easily scalable
  - Deposit directly onto electroformed shell
- Cost effective and efficient
- Established industry base, does not require large capital expense for application



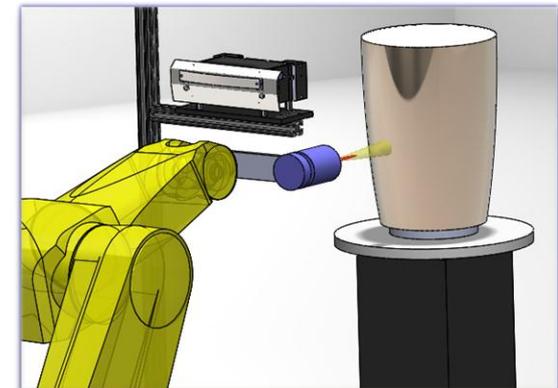
Multilayers

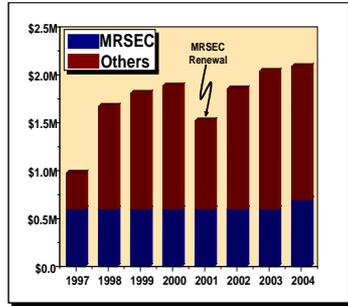


Composites/Cermets



Graded Coatings





**Value Added Benefits from Core NSF Funding**



*Consortium is operated by the Center for Thermal Spray Research at Stony Brook University*



Stony Brook-Caterpillar Team



**ReliaCoat Technologies** *Founded May 2009*

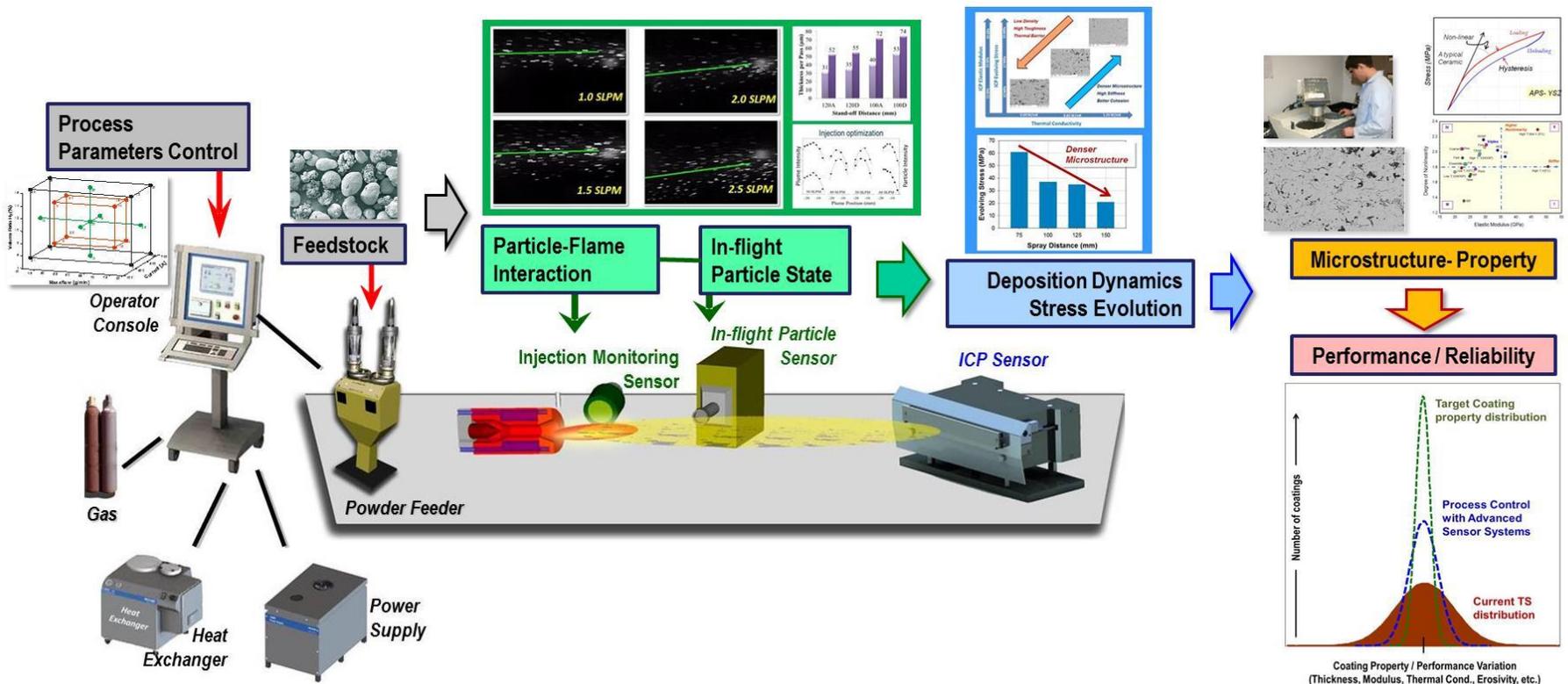
**Advanced tools, software, and technology services company**



**Expanded to new location Summer 2012**







**Particle State**

- Particle Velocity
- Kinetic Energy
- Fluid dynamics
- Particle Temperature
- Oxidation/decomposition
- Rapid cooling/phase transformations

**Local Deposition Temperature**

- Intersplat bonding strength
- Wetting/ adsorbate-condensates
- Residual Stress (quenching-peening)

**Materials intrinsic Properties**

- Substrate-splat – adhesion interface
- Splat-splat-intersplat interfaces
- Interpass interfaces
- Elastic –plastic behavior
- High strain – strain rates
- Heat transfer



## Material Compatibility

- Thermal mismatch

## Minimal Coating Residual Stress

- Separated optic shape retention

## Coating Adhesion

- Bond strength

## Minimize Thermal Input to Mandrel

- Figure accuracy

## No Damage from Particle Impact

- Optical surface distortion

## Environmental Considerations

- Vacuum
- Outgassing



Defined Challenges	Proposed Mitigation Strategies
Light weight, rigid & high toughness carrier layer	<ul style="list-style-type: none"><li>▪ Base structure of Al<sub>2</sub>O<sub>3</sub> or other porous ceramic coating</li><li>▪ Al<sub>2</sub>O<sub>3</sub>-Aluminum composite/functionally graded structure</li></ul>

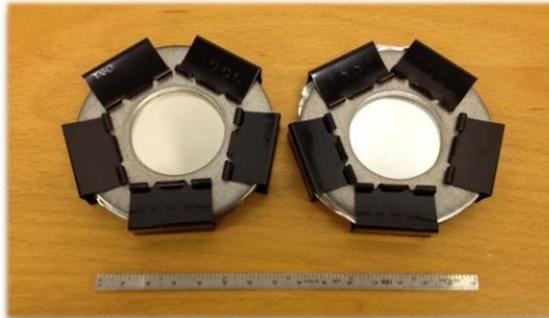




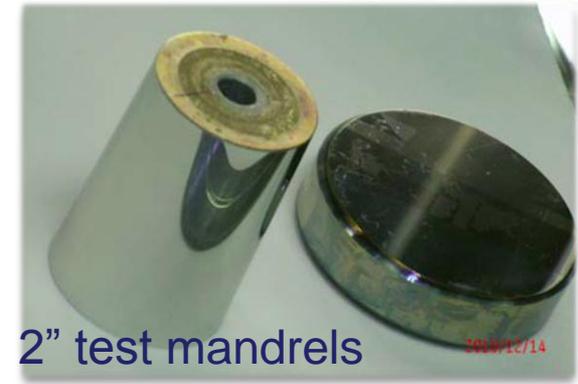
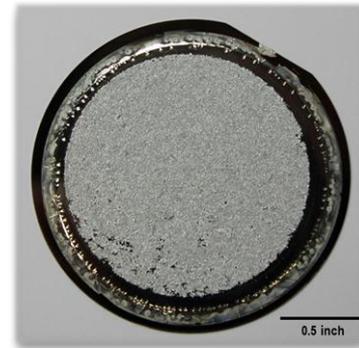
Aluminum Powder

Fine powder size to minimize particle energy

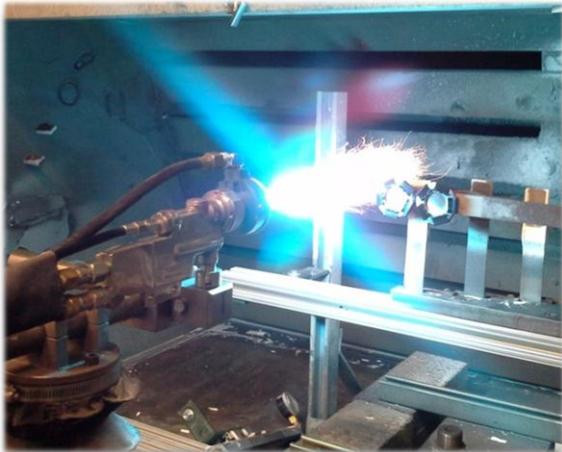
Initial Test Substrates



Evaluate potential particle damage using nickel and aluminum foil



2" test mandrels



Flame Spray



Plasma Spray

Process development using NiCo plated silicon wafers (due to mandrel availability), continued testing on flat and conical mandrels to evaluate X-ray performance



X-ray reflectivity measurements

